

Use of HWD (deflection), Backcalculation, and Multilayer Elastic Analysis for Airport Pavement Evaluation

Prepared by:
Khaled Galal, Ph.D.
Pavement & Materials
Research Team Leader
Stantec Consulting
Charlotte, NC

Presented by:
Leanne Whiteley-Lagace,
M.A.Sc., P.Eng.
Pavement Engineer
Stantec Consulting
Hamilton, ON

One Team. Infinite Solutions



SWIFT 2010
Calgary, AB

Acknowledgements

- Greater Moncton International Airport
- Hatch Mott MacDonald

Presentation Outline

- Project Background
- Supplemental Research Work
- FWD, Backcalculation, & ELT
- Case Study
- Decision Tree (Rehab Options)
- Evaluation
- Conclusions & Recommendations

Project Background

Scope & Objectives

- 3-year airside pavement improvement program
- Year 1 program
 - Taxiway 'A'
 - Apron V
 - Apron I (northern two-thirds)
 - Runway 11-29 (300 m beginning at the western end)
- Objective
 - Determine the existing pavement structure
 - Analyze the structure in terms of pavement strength
 - Develop recommendations for rehabilitation

Project Background

Pavement Evaluation

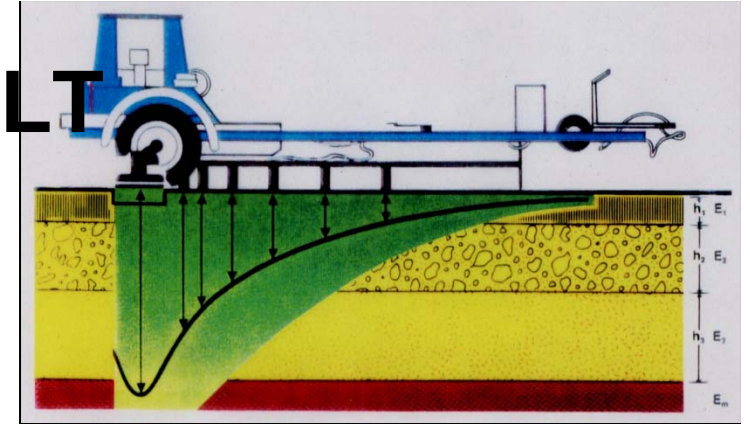
- Series of 14 boreholes (BH)
 - To determine pavement structure and layer types
- Dynamic Cone Penetrometer (DCP) at 5 BH
 - To determine the strength of the granular layer underlying the pavement surface
- Visual distress survey
 - To assess surface distress condition
- Heavy Weight Deflectometer (HWD) survey
 - To determine pavement structural strength



Supplemental Research Work

- New methodology developed within Stantec, to develop and evaluate rehabilitation options
 - FWD Analysis
 - Backcalculation
 - Multi-layer elastic analysis
- Case Study
 - Runway 11-29

FWD, Backcalculation, & ELT Pavement Evaluation

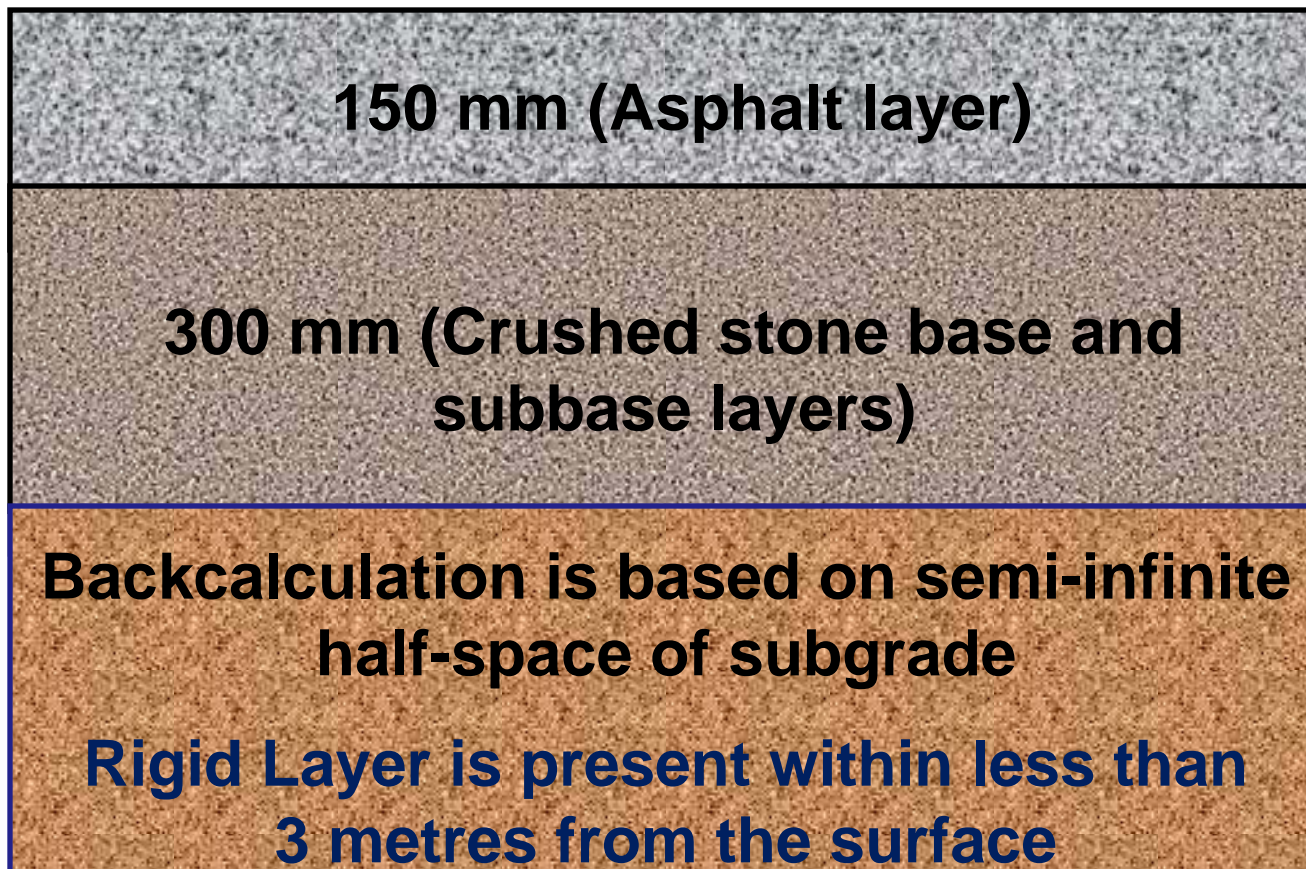


- FWD Analysis
 - Determine in-situ structural capacity of the pavement structure (and subgrade soil conditions)
- Backcalculation
 - Procedure to determine Young's modulus of Elasticity for pavement materials, using measured surface deflections by working elastic layer theory "backwards"
- Elastic Layer Analysis
 - Measurement of deflections, stresses, and strains

Case Study

Runway Structure

| Avg. Core Thicknesses | |
|-----------------------|---------|
| AC | Crushed |
| 5.9 | 11.8 |



Case Study

FWD & Backcalculation

HWD Inputs

- 2 drops at each load level
- 3 load levels
 - 60 kN (13,500 lbf)
 - 90 kN (20,200 lbf)
 - 120 kN (27,000 lbf)

HWD Analysis Outputs

- E1 - modulus of asphalt layer
- E2 - modulus of the base/subbase layer
- E3 - modulus of the subgrade layer
- Statistics - Average, Standard deviation, Maximum, Minimum, Coefficient of Variance

Case Study

Backcalculation: Layer 1 - Asphalt

| Drop No. | Stress (kPa) | Load (kN) | E1 (MPa) | | | | |
|--------------------|--------------|-------------|--------------|-------|-------|-------|-------|
| | | | Avg | StDev | Max | Min | COV |
| 1 | 859 | 61 | 3,393 | 1,364 | 6,171 | 1,630 | 40.2% |
| 2 | 1362 | 96 | 3,415 | 1,214 | 6,043 | 1,835 | 35.5% |
| 3 | 1793 | 127 | 3,582 | 1,411 | 6,372 | 1,900 | 39.4% |
| 4 | 865 | 61 | 3,621 | 981 | 5,061 | 2,149 | 27.1% |
| 5 | 1274 | 90 | 3,704 | 1,073 | 5,570 | 2,106 | 29.0% |
| 6 | 1694 | 120 | 3,645 | 1,151 | 5,695 | 2,085 | 31.6% |
| Overall Avg | | 92.5 | 3,560 | | | | |

| Drop No. | Stress (psi) | Load (lbf) | E1 (psi) | | | | |
|--------------------|--------------|---------------|----------------|---------|---------|---------|-------|
| | | | Avg | StDev | Max | Min | COV |
| 1 | 125 | 13,646 | 492,044 | 197,812 | 894,988 | 236,415 | 40.2% |
| 2 | 197 | 21,636 | 495,368 | 176,068 | 876,494 | 266,077 | 35.5% |
| 3 | 260 | 28,498 | 519,567 | 204,660 | 924,148 | 275,609 | 39.4% |
| 4 | 126 | 13,752 | 525,117 | 142,271 | 734,007 | 311,704 | 27.1% |
| 5 | 185 | 20,241 | 537,172 | 155,556 | 807,897 | 305,437 | 29.0% |
| 6 | 246 | 26,917 | 528,682 | 166,980 | 826,027 | 302,356 | 31.6% |
| Overall Avg | | 20,782 | 516,325 | | | | |

Asphalt layer is in fair to good condition

Case Study

Backcalculation: Layer 2 – Base/subbase

| Drop No. | Stress (kPa) | Load (kN) | E1 (MPa) | | | | |
|--------------------|--------------|-------------|--------------|-------|-------|-----|-------|
| | | | Avg | StDev | Max | Min | COV |
| 1 | 859 | 61 | 3,799 | 3,164 | 9,282 | 417 | 83.3% |
| 2 | 1362 | 96 | 3,907 | 2,496 | 7,402 | 650 | 63.9% |
| 3 | 1793 | 127 | 4,260 | 2,901 | 7,706 | 726 | 68.1% |
| 4 | 865 | 61 | 4,223 | 2,827 | 8,374 | 761 | 67.0% |
| 5 | 1274 | 90 | 3,819 | 2,570 | 7,441 | 774 | 67.3% |
| 6 | 1694 | 120 | 4,254 | 2,819 | 8,442 | 839 | 66.3% |
| Overall Avg | | 92.5 | 4,044 | | | | |

| Drop No. | Stress (psi) | Load (lbf) | E1 (psi) | | | | |
|--------------------|--------------|---------------|----------------|---------|-----------|---------|-------|
| | | | Avg | StDev | Max | Min | COV |
| 1 | 125 | 13,646 | 550,962 | 458,901 | 1,346,201 | 60,436 | 83.3% |
| 2 | 197 | 21,636 | 566,601 | 361,988 | 1,073,602 | 94,264 | 63.9% |
| 3 | 260 | 28,498 | 617,822 | 420,988 | 1,117,672 | 105,280 | 68.1% |
| 4 | 126 | 13,752 | 612,501 | 410,064 | 1,214,612 | 110,308 | 67.0% |
| 5 | 185 | 20,241 | 553,850 | 372,742 | 1,079,249 | 112,279 | 67.3% |
| 6 | 246 | 26,917 | 616,968 | 408,793 | 1,224,462 | 121,677 | 66.3% |
| Overall Avg | | 20,782 | 586,451 | | | | |

Increased base/subbase modulus due to compensation effect of rigid layer

Case Study

Backcalculation: Layer 3 – Subgrade

| Drop No. | Stress (kPa) | Load (kN) | E1 (MPa) | | | | |
|--------------------|--------------|-------------|------------|-------|-----|-----|-------|
| | | | Avg | StDev | Max | Min | COV |
| 1 | 859 | 61 | 384 | 175 | 547 | 151 | 45.5% |
| 2 | 1362 | 96 | 394 | 166 | 567 | 133 | 42.2% |
| 3 | 1793 | 127 | 398 | 133 | 566 | 210 | 33.4% |
| 4 | 865 | 61 | 360 | 183 | 612 | 174 | 50.9% |
| 5 | 1274 | 90 | 401 | 158 | 576 | 222 | 39.4% |
| 6 | 1694 | 120 | 393 | 154 | 581 | 209 | 39.1% |
| Overall Avg | | 92.5 | 388 | | | | |

| Drop No. | Stress (psi) | Load (lbf) | E1 (psi) | | | | |
|--------------------|--------------|---------------|---------------|--------|--------|--------|-------|
| | | | Avg | StDev | Max | Min | COV |
| 1 | 125 | 13,646 | 55,711 | 25,360 | 79,395 | 21,964 | 45.5% |
| 2 | 197 | 21,636 | 57,090 | 24,109 | 82,237 | 19,296 | 42.2% |
| 3 | 260 | 28,498 | 57,699 | 19,279 | 82,056 | 30,512 | 33.4% |
| 4 | 126 | 13,752 | 52,182 | 26,573 | 88,768 | 25,248 | 50.9% |
| 5 | 185 | 20,241 | 58,179 | 22,907 | 83,545 | 32,144 | 39.4% |
| 6 | 246 | 26,917 | 57,065 | 22,324 | 84,224 | 30,368 | 39.1% |
| Overall Avg | | 20,782 | 56,321 | | | | |

Higher variability is an indication of inconsistent layer

Decision Tree (Rehab Options)

If surface condition is **very poor to poor**

Rehab Options:

1. Hot in place recycling of the existing asphalt and overlay with a new HMA high stiffness surface layer (SMA* or Superpave* with PG 70-34* or PG 76-34* or equivalent)
2. Total reconstruction

* Use 1.5% lime by weight for high stiffness HMA Use 0.3 - 0.5 AC% above optimum for durability
Consider use of warm asphalt mix technology

Decision Tree (Rehab Options)

If surface condition is **poor to fair**

Rehab Options:

1. Mill 80 mm (3 in) of existing asphalt and overlay with a 125 mm (5 in) of HMA high stiffness surface layer (SMA* or Superpave* with PG 70-34* or PG 76-34* or equivalent)
2. If milling is not an option, then overlay 125-180 mm (5 -7 in) after surface sealing & repair

Decision Tree (Rehab Options)

If surface condition is **fair to good**

Rehab Options:

1. Mill 50 mm (2 in) and overlay 80 mm (3 in) of HMA high stiffness surface layer (SMA* or Superpave* with PG 70-34* or PG 76-34* or equivalent)
2. If milling is not an option, then overlay with 50 mm (2 in) after surface sealing & repair

Decision Tree (Rehab Options)

If surface condition is **good to very good**

Rehab Options:

1. Mill 25 mm (1 in) and overlay with 50 mm (2 in) of HMA high stiffness surface layer (SMA* or Superpave* with PG 70-34* or PG 76-34* or equivalent)
2. If milling is not an option, then overlay 40-50 mm (1.5-2 in)

Evaluation

Rating Criteria - Scale

- 1 – 5 Rating Index Scale
 - Rating Index 5 = very good
 - Rating Index 4 = good
 - Rating Index 3 = fair
 - Rating Index 2 = poor
 - Rating Index 1 = very poor

Evaluation

Rating Criteria – Functional vs. Structural

- Functional conditions
 - Based on surface distress
- Structural conditions
 - Based on Backcalculation
 - Based on Multilayer Elastic Analysis Results
 - To reduce pavement deflection and tensile strain at bottom of asphalt layer under main gear of the design aircraft
 - Reduce surface deflection as follows:

Evaluation

Rating Criteria – Deflection Performance

- Deflection vs. Strain Relationship
 - 25 microns (4 mils) or less = Very good
 - 100 – 150 microns (4 – 6 mils) = Good
 - 150 – 200 microns (6 – 8 mils) = Fair
 - 200 – 250 microns (8 – 10 mils) = Poor
 - 250 microns (10 mils) or higher = Very Poor

Evaluation

Results

- FWD Analysis
 - Avg. deflection = 192 microns (7.9 mils)
 - Standard deviation = 53 microns (2.1 mils)
- Multilayer Elastic Analysis
 - Low subgrade deflection
 - Less than 120 micro strains for the tensile strain at the bottom of the asphalt layers

Indicating fair to good runway condition

Conclusions & Recommendations

- Rating Index = 3 - 4 (fair to good)
 - Based on calculations and visual inspection
- Rehab Options
 - Mill 50 mm (2 in) and overlay 80 mm (3 in) of HMA high stiffness surface layer (SMA* or Superpave* with PG 70-34* or PG 76-34* or equivalent)
 - If milling is not an option, then overlay with 50 mm (2 in) after surface sealing & repair

Conclusions & Recommendations

- To replace SMA/Superpave, recommend performance grades (PG):
 - Use 1.5% lime by weight for high stiffness HMA
 - Improve stiffness
 - Prevents stripping potential
 - Reduces rutting potential
 - Use 0.3 - 0.5 AC% above optimum
 - Improve durability, i.e. reduce cracking potential
 - Consider use of warm asphalt mix technology
 - Similar to Boston Logan International taxiway

Questions

Khaled A. Galal, Ph.D.
Pavement & Material
Research Team Leader

2127 Ayrley Town
Boulevard Ste. 300
Charlotte NC 28273
Ph: (980) 297-7655
Fx: (704) 329-0905
Cell: (980) 225-3077
Khaled.Galal@stantec.com

Leanne Whiteley-Lagace,
M.A.Sc., P.Eng.
Pavement Engineer

1400 Rymal Road East
Hamilton ON
Ph: (905) 381-3243
Fx: (905) 385-3534
Cell: (289) 339-1749
Leanne.WhiteleyLagace
@stantec.com